

A "high entropy" alloy database TCHEA2

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1. Calphad and TCHEA2

2. Models and modeling

3. Prediction of Phase formation

4. Application in alloy design

Why Calphad?



- **Empirical rules** (Hume-Rothery rule and the like)
- Theoretical first principles method
- Semi-empirical Calphad method

Calphad+++

• **Considering** specific systems, specific structures, specific compositions, various intermetallics, solutions bases on intermetallics

Predicting

- which SSSs to form, and its composition and temperature ranges
- \circ if, when and where it orders
- \circ if, when and where it decomposes
- which intermetallics to form and the phase amounts
- \circ the coexistence and competitions of several SSSs
- the promising/coherent/semicoherent intermetalics
- 0 ...
- Aided by theoretical first principles method

Calphad+++

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Calphad: Thermodynamics & kinetics





TCHEA: CCAs/MPEAs, inkl. HEAs





TCHEA2

- **20** element framework
- 185 binaries assessed
- 443 ternaries assessed
- □ ALL solid phases in assessed systems

Highlight

- Compounds of the same structure are modelled as the same phase and the mutual solubility considered, e.g. Sigma
- Partitioning models for BCC and FCC (order/disorder)





Raymundo Arroyave (Texas A & M University)

- 216 HEAs
- 85 % on target



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- Substitutional phases
- Liquid, Fcc_A1, Bcc_A2, Hcp_A3, & more

$$G^{\emptyset} = \sum_{i}^{n} x_{i} G_{i}^{\emptyset} + RT \cdot \sum_{i}^{n} x_{i} \ln(x_{i}) + \sum_{i=1}^{n-1} \sum_{j=i+1}^{n} x_{i} x_{j} L_{ij}$$
$$+ \sum_{i=1}^{n-2} \sum_{j=i+1}^{n-1} \sum_{k=j+1}^{n} x_{i} x_{j} x_{k} L_{ijk}$$

(Eq 1)

- To reliable extrapolate into
- high-order systems
- metalstable compositional ranges
- Bin. & Tern. interaction parameters are crucial



- Sublattice models
- o Intermetallic compounds & solutions based on them
- Most with 2SL and 3SL models

$$G^{\emptyset} = \sum_{i=1}^{m} \sum_{j=1}^{n} y_{i}^{(1)} y_{j}^{(2)} G_{i;j}^{\emptyset} + RT$$

$$\cdot \left(2 \cdot \sum_{i}^{m} y_{i}^{(1)} \ln(y_{i}^{(1)}) + \sum_{i}^{n} y_{i}^{(2)} \ln\left(y_{i}^{(2)}\right) \right)$$

$$+ \sum_{i=1}^{m-1} \sum_{j=i+1}^{m} \sum_{k}^{n} y_{i}^{(1)} y_{j}^{(1)} y_{k}^{(2)} L_{ij:k} \qquad (Eq 2)$$

$$+ \sum_{i=1}^{n-1} \sum_{j=i+1}^{n} \sum_{k}^{m} y_{k}^{(1)} y_{i}^{(2)} y_{j}^{(2)} L_{k:ij}$$

$$+ \sum_{i=1}^{m-1} \sum_{j=i+1}^{m} \sum_{k=1}^{n} \sum_{l=k+1}^{n-1} y_{i}^{(1)} y_{j}^{(1)} y_{k}^{(2)} y_{l}^{(2)} L_{ij:kl}$$



- Partitioning models
- Fcc_L12 + Fcc_A1
- \circ Bcc_B2 + Bcc_A2



 $G_m = G_m^{dis}(x_i) + G_m^{ord}(y_i^s)$



• Sigma, ...





(A, B, ...)

hypothetical sigma solution

 $(Eq \ 4)$

Gibbs energy of the fictitious disordered structure Contribution from ordering parameters

Molar volume



- **molar volume** and its temperature and composition dependence
- experimental data of densities, lattice parameters, and thermal expansivity and/or theoretical values
- recalculation of volume & volume fraction, density, expansivity, shrinkage during casting, lattice parameters & lattice misfit

$$V = V_0 \cdot exp\left(\int_{T_0}^T 3\alpha dT\right)$$

Redlich-Kister expansion

$$V_m = x_A V^A + x_B V^B + x_A x_B \cdot V^{A,B}$$

$$V_m = x_A V^A + x_B V^B$$

Vegard's law

$$V_{m} = \sum_{i=A}^{B} \sum_{j=A}^{B} y_{i}^{(1)} y_{j}^{(2)} V^{i:j} + \sum_{i=A}^{B} y_{i}^{(1)} y_{A}^{(2)} y_{B}^{(2)} \cdot V^{i:A,B} + \sum_{i=A}^{B} y_{A}^{(1)} y_{B}^{(1)} y_{j}^{(2)} \cdot V^{A,B:j}$$

Sublattice model



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Prediction of Phase formation



□ Heat treatment (homogenization, aging, etc.)

Solidification

- Phases
- Phase formation sequence
- Phase fractions
- Phase compositions
- Phase reactions
- Phase transition temperatures
- Composition microsegregation

Solidification simulations

- Using TCHEA and Thermo-Calc
- Equilibrium calculation
- Scheil (non-equilibrium) calculation

Assumption for Scheil: the diffusion in liquid is extremely fast while that in solid phases is extremely slow







2012MaSG-MSEA480, Arc melt Al<u>CoCrFeNi</u>-0.10Nb

Co-Cr-Ni



Fcc_A1 @ Co1Cr1Ni1

- Competition from Sigma
- Competition from Bcc_A2



CoCrFeNi

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Fcc_A1 single @ Co1Cr1Ni1Fe1



CoCrFeNi-Al



The phase formation depends on experimental conditions, especially cooling rate and heat treatment.



2008Zhang-AdvEngMater534

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FCC in as-cast Al0.5CrFeCoNi

2009Chou-MSEB184

as-cast alloys, heated @ +10 C/min to 1100 C, stayed for 24 h.

- x = 0-0.375 FCC
- x = 0.5 1.0 FCC + BCC
- x = 1.25 2.0 BCC

2009Kao-JAlloyComp57

as-cast alloys, heated @ +20 C/min to 1100 C, stayed for 24 h.

- x = 0-0.375 FCC
- x = 0.5 0.75 FCC+BCC
- x = 0.875 2.0 BCC

CoCrFeNi-0.1Al

He (2017)

- Single Fcc_A1 is metastable @ 750 °C
- Decomposition after 800 h (2nd FCC)





- Calculation: 2.65% Bcc_A2 instead of a 2nd A1
- NI 2.85033E-01
- AL 2.26551E-01
- CR 7.66706E-02
- CO 2.27997E-01
- FE 1.83749E-01
- Not in miscibility gap
- 0.3670 nm A1
- 0.2924 nm A2

 $\sqrt{2} \cdot a = 0.413$ nm

He et al., Scr. Mater. 126 (2017) 15-19

CoCrFeNi-0.65Al (13.98 at.% Al)



- 2-phase eutectic reaction is not invariant
- Segregation can be significant



Solidification simulation of the eutectic alloy $Co_1Cr_1Fe_1Ni_1Al_{0.65}$: (a) phase formation sequence and solid phase fractions from equilibrium (in dashed line) and Scheil simulation (solid line); and (b) liquid phase composition from Scheil simulation

CoCrFeNi-1Al





2012Wang-Intermetallics44

As-cast: BCC_B2
 2009Chou-MSEB184

+10 C/min to 1100 C, held for 24 h

BCC + FCC

2009Kao-JAlloyComp57

+20 C/min to 1100 C, held for 24 h

BCC

2016Munitz-JAlloysCompd683

As-cast: BCC_B2 + BCC_A2



Simplifications

- Back diffusion in Bcc_B2
- Composition segregation in liquid

CoCrFeNi-1Al



- Step-by-step Scheil simulation
- Step size: 4 K



CoCrFeNi-Cu



- 2005Tong-MetMaterTransA881
- 2 Fcc_A1 phases @ Co1Cr1Cu1Fe1Ni1



as-cast, 1 to 10 K/s



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Alloy composition map





CoCrFeNi + Re vs Ru



Fcc_A1 to Hcp_A3



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CoFeReRu

2016Gao-MMTA47 As-cast



 \mathbb{A}





Co-Fe-Re-Ru

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2016Gao-MMTA47



0.45

Co-Fe-Re-Ru

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Co-Fe-Re-Ru-X



- No experimental investigations
- o Ni





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